

GTV Spray powder catalogue

Application fields

Overhaul / Repair

Wear protection

Corrosion protection

Bond Coats

Electrical isolation

Thermal isolation

Clearance control (Abradable coatings)

Powder morphology

Fused and crushed powder

Water or gas atomized powder

Agglomerated and sintered powder

Clad powder

GTV spray powders comply with DIN EN 1274

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Application fields

The technology of thermal spraying permits the manufacturing of adapted surfaces for each application by local deposition of coating materials with optimized properties. Due to the various possibilities to combine coating and substrate materials and due to the large variety of processes and achievable processing conditions, thermal spraying is of utmost significance among the coating processes. In various applications it offers perfect solutions regarding surface technological problems.

The majority of thermal spray applications can be found within the following outlined fields. In practice these fields often overlap. Therefore a multiplicity of proven coating materials exceed the property profile necessary within individual applications.

Overhaul / Repair

Technical components are not only subject to changes of shape by wear, but also show deviations due to manufacturing tolerances. Regardless whether cast, forged, sheet metal or machined parts are concerned the various thermal spray processes offer application-adapted possibilities for the restoration of faulty components.

The universal spectrum of spraying consumables offered by GTV enables the customer to select the material either depending on the load or with regard to the compatibility of the coating and substrate material.

Wear protection

The optimal choice of a coating material for wear protection of component surfaces depends on the tribological system (materials and surface state of the friction partners, relative movement, lubrication, load). The friction condition can be liquid, boundary or dry friction. Also, in accordance with the chemico-physical boundary conditions different wear mechanisms can occur: abrasion, adhesion, fatigue and / or tribo-chemical reaction.

Abrasion takes place through scratching of the component surface by a substantially harder counterbody or during the interaction with a fluid that contains abrasive particles. Hard, dense and fine-structured coatings have proved to be best suited for this type of tribological conditions. In case of interaction with a fluid that contains abrasive particles the size of hard phases in e.g. WC/Co(Cr) or $\text{Cr}_3\text{C}_2/\text{Ni20Cr}$ coatings has to be adapted to the abrasive particles size in order to provide optimal wear protection function by avoiding local removal of the soft binder phase. Depending on the specific tribological load the spectrum of GTV spraying consumables offers adequate solutions with adapted hardness, hard phase size and distribution within a matrix material and resistance to impact load. In addition to the wear resistance of the coating material one has to consider the kind of applicable finishing and the achievable coating thickness required to ascertain an aspired life time.

Adhesion wear proceeds by formation and destruction of atomic bonds (micro or cold weldings) between the friction partners resulting in tear out of material from one components surface and transfer to the counterbody. Adhesion wear, also called "galling", can be avoided by the use of coatings with low adhesion properties (low surface energy) or adapted lubricating and / or sliding characteristics.

Fatigue wear occurs as consequence of cyclic mechanical or thermo-mechanical load. Accumulative plastic deformation within micro contact areas leads to excess of the materials strain capability and therefore to crack evolution. Crack propagation under ongoing cyclic load finally leads to material removal from the component surface. As crack evolution can originate from microstructure irregularities like pores, phase and grain boundaries that are generally present in thermal spray coatings, a coating designed to resist fatigue wear has to provide high fracture toughness in order to prevent excessive crack propagation. Homogeneous and dense coatings with compressive residual stress state show best suitability for this type of tribological conditions.

The *tribo-chemical reaction* is as a chemical reaction occurring during and due to the tribological load leading to material loss in form of reaction products on one or both friction partners. Tribo-chemical reactions are favored by friction induced rise of (local) temperature. Reaction products like e.g. metal oxides differ from the base material concerning hardness, strain capability, thermal expansion and thermal shock behavior. In the shape of fine particles these oxides can additionally affect the tribological conditions, e.g. by superposition of abrasive wear. Thermal spray coatings protecting component surfaces efficiently against wear due to tribo-chemical reactions need to be chosen under consideration of the environment and the counterbody's chemical composition.

In practice the described wear mechanisms often occur superimposed. E.g. sliding, rolling and oscillation wear can impart all of the described mechanisms simultaneously. Beyond that the prevailing application temperature can substantially influence the material behavior. Therefore spraying feedstock that permits production of coatings that fulfill the sum of partially contradicting demands according to the complex tribological conditions in an optimal way have to be chosen.

Corrosion protection

Adequate choice of feedstock for production of corrosion protective coatings requires consideration of the substrate's chemical properties, the environment in use of the component as well as pressure and temperature in use of the component. Furthermore attention has to be paid whether the corrosion attack is pure based on chemical or electro-chemical reactions. In particular for electro-chemical corrosion attack the influence of potentially existing contact materials, e.g. due to partial coating of the component's surface, needs to be taken into account. Choice of a coating material that is more noble than the substrate material can even lead to accelerated corrosion, if there is a location, where the corrosive medium can penetrate the coating down to the substrate surface.

Corrosive attack on the substrate material by the surrounding medium via pure chemical corrosion processes can be prevented by application of chemically more resistant coatings. Also there is the possibility to produce cathodically protective coatings. In that case the less noble coatings corrode instead of the substrate material and thereby provide protective function. Typical examples are zinc and aluminum coatings on steel structures.

Electro-chemical corrosion takes place, if two materials showing substantially dissimilar corrosion potential are in contact by a conductive liquid film. Coatings suppressing the galvanic current flow are utilized to prevent this type of corrosion.

Bond coats

Bond coats are sprayed as intermediate layers with the aim to improve the adhesion of a functional coating to the substrate. Besides molybdenum that permits local formation of metallurgical bonds at impact of liquid spray particles on the substrate surface due to the materials high reactivity and high melting temperature the spectrum of so called self bonding coatings provides high adhesion strength. Therefore such coatings are an excellent base for thermally sprayed functional coatings. For production of self bonding coatings clad powders are used. The powder constituents undergo an exothermic reaction and therefore impinge on the substrate at significantly higher temperature than particles sprayed with homogeneous alloy particles with the same chemical composition. Diffusion processes lead to a local formation of metallurgical bonds. But self bonding coatings are not only used as bond coats. They are also available with different hardness levels and can be used as functional coatings, e.g. for combined wear and corrosion protection.

A further group of bond coats are ductile nickel or cobalt based alloys that prevent access of corrosive media to the substrate surface, if functional top coats cannot provide this function securely. Hot gas corrosion protective MCrAlY (M := Ni, Co) coatings are also designed in a way that they show an intermediate thermal expansion behavior between typical super alloy substrates and zirconia based thermal barrier top coats. Therefore thermally induced strain is minimized and thermal shock resistance of the compound greatly improved. Such coatings can provide excellent long-term oxidation resistance up to 1,050 °C.

Electrical isolation

In various applications special electrical characteristics of thermally sprayed coatings are utilized. Thus by the use of non conductive ceramic coatings with high dielectric strength the conduction of electric currents between technical components is prevented. In contrast other applications require the use of coatings with particularly high electrical conductivity, e.g. copper or aluminum).

Thermal isolation

Due to extreme thermal loads various components in modern technical systems have to be coated with so called thermal barrier coatings. Apart from decreased component core temperatures that result in increased life time the process efficiency can be increased at constant component core temperature, because either the operating temperature can be increased or the cooling capacity reduced.

Usually ceramics are applied as thermal barrier coating materials. Especially oxide ceramics mostly show low thermal conductivities. If the coatings are also subject to thermal cyclic loads the use of ceramics with a comparatively high coefficient of thermal expansion and thermal shock resistance is essential.

Clearance control (Abradable coatings)

Tolerances in the interaction of turning and static components have to be kept as small as possible to achieve optimum process efficiencies of e.g. power generation systems. Thus power losses can be substantially decreased by keeping close clearances, e.g. in gas turbines or screw compressors.

By combination of „abradable“ coatings, often applied upon static components, with wear resistant coatings applied to turning components, the resistant material successively grates into the abradable. Thereby a minimum clearance between the components is attained.

Powder morphology

Due to the diversity of processes and spraying materials the technology of thermal spraying offers adapted solutions for a wide range of application fields. GTV offers the full spectrum of feedstock powder with different morphology, size fractions and chemical composition. Thereby the user is enabled to exploit the full potential of the thermal spray technology.

Spraying powder are available in very different size fractions and with different morphologies. Both properties take significant influence e.g. on the flowing characteristics, the melting behavior and potential micro-structural transformations during the spraying process or subsequently performed heat treatments.

The consequence of bad powder flow characteristics are fluctuations in powder feeding and thereby induced inhomogeneities in the produced coatings microstructure. Therefore, even for use of fine powder size fractions minimum flow characteristics need to be maintained.

The melting behavior has to be evaluated with regard to the desired heat transfer into the powder particles. The degree of melt formation in single particles determines e.g. the intensity of chemical reactions like oxidation or reactions of different powder constituents as well as phase transformations during spraying.

The powder particles morphology is a result of the powder production route and the applied processing. The majority of common spray powders is produced via four different routes.

Fused or sintered and crushed powders

Such powders are produced by crushing of a cast or sintered block and subsequent milling to achieve a desired particle size regime.

This procedure is mainly used for brittle materials like oxide-ceramics or carbides. The particles are characterized by a comparatively high density and a moderate melting behavior.

To manufacture multi-component powders with individual constituents side by side the raw materials are mixed and afterwards bonded by means of sintering. Finally the sintered block is crushed and milled.

Crushed powder particles show a rough, fissured surface and irregular shape (**figure 1**) which leads to rather poor flow characteristics.

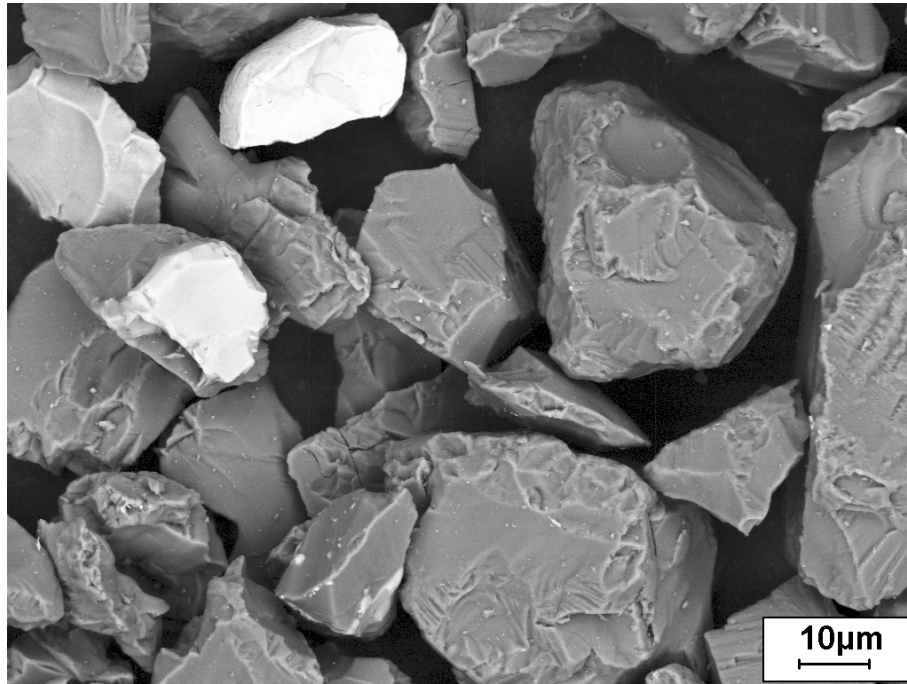


Figure 1: Scanning electron micrograph of a fused and crushed $\text{Al}_2\text{O}_3/\text{TiO}_2$ 97/3 powder

Water or gas atomized powders

Production of atomized powders proceeds by atomization of molten material with use of adapted atomization gases either into water pool or into a vessel with adapted gas atmosphere. By choice of the atomizing gas and the atmosphere the material composition can be influenced, e.g. with concern to the powders oxygen content. Thus, the hardness of a molybdenum coatings can be controlled not only by the spraying conditions, but also by the oxygen content of the powder feedstock. On the other hand the oxygen content in MCrAlY powders is kept at minimum values in order to permit spraying of coatings that will show optimized oxidation resistance.

Particles of water or gas atomized powders show a relatively low surface roughness. Water atomized particles show a more irregular geometry (**figure 2**), while gas atomized particles are nearly perfectly spherical (**figure 3**). The spherical shape greatly supports the flowing behavior. Due to the minimal surface / volume ratio of the sphere shape the heat flux into the particles and therefore the melting behavior is impeded.

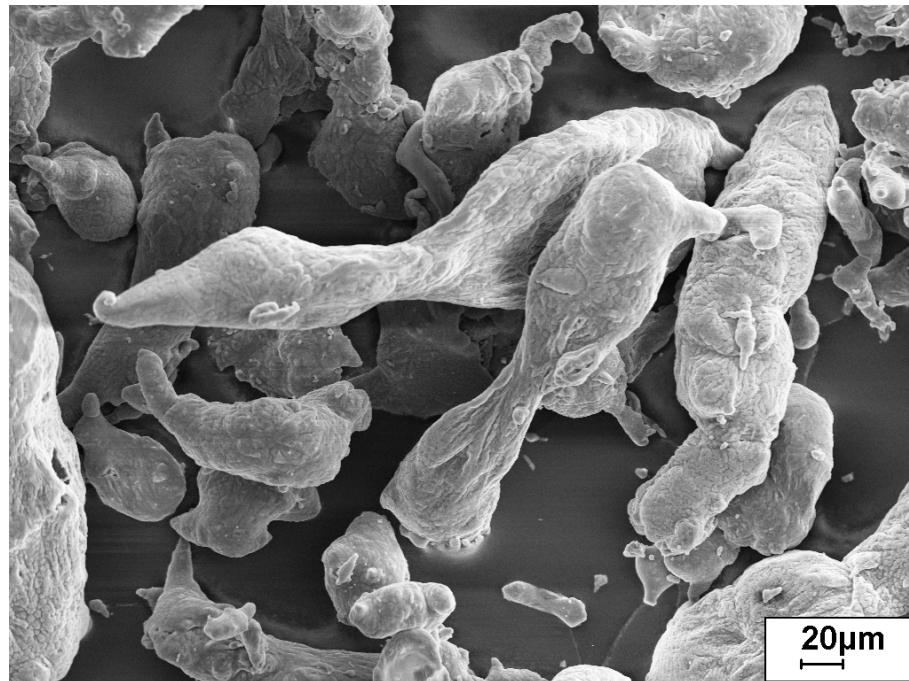


Figure 2: Scanning electron micrograph of a *water atomized* aluminum powder

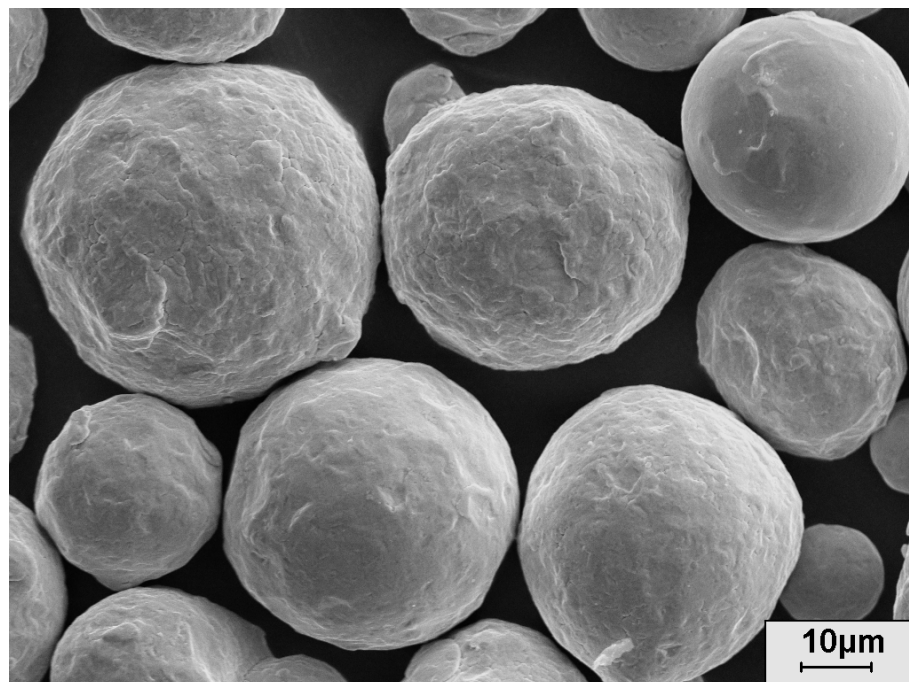


Figure 3: Scanning electron micrograph of a *gas atomized* Ni20Cr powder

Agglomerated and sintered powders

Due to a large surface / volume ratio agglomerated and sintered powders show excellent melting behavior. Their flowing characteristics are relatively good due to nearly spherical shape of most particles (**figure 4**).

Powders are produced by atomizing a suspension containing one or more material constituents as well as an organic binder into a large vessel that is kept at constant elevated temperature. Thereby spherical agglomerates are formed. The process is well established for manufacturing of cermet powders, but oxide powders are also produced. In order to avoid particle break up due to high shearing forces acting in the spray jet, in particular in the high velocity flames of HVOF guns, the agglomerates are densified in either a thermal plasma jet or in a sintering furnace. In addition, during the densification process the organic binder that would affect thermal spray coatings mechanical properties is eliminated.

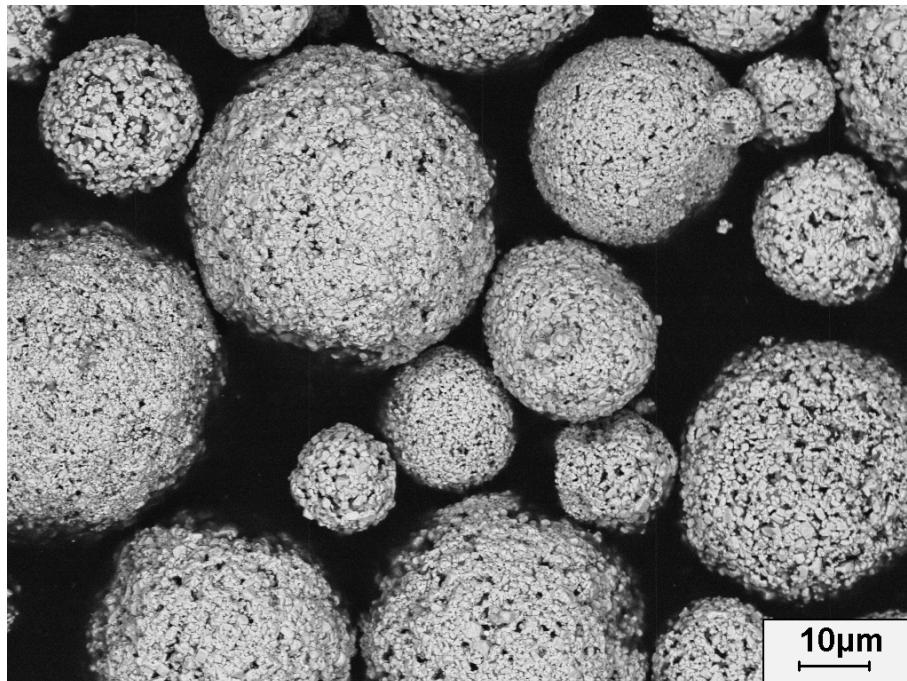


Figure 4: Scanning electron micrograph of an *agglomerated and sintered WC/Co 88/12* powder

Clad powders

To protect specific material constituents of compound powders against direct contact with the heat source of a thermal spray process or to take influence on chemical reactions of the powder constituents several powders clad.

CVD and sol gel processes are used as well as electrolytic coating processes. Furthermore adapted milling processes permit a so called mechanical cladding. Finally relatively coarse core particles are clad by fine powder particles of another constituent by use of an organic binder (**figure 5**). Like in the case of agglomerated and sintered powder the composite strength can be improved by annealing. Thereby it is important not to initiate chemical reactions that are desired to occur only in the spraying process.

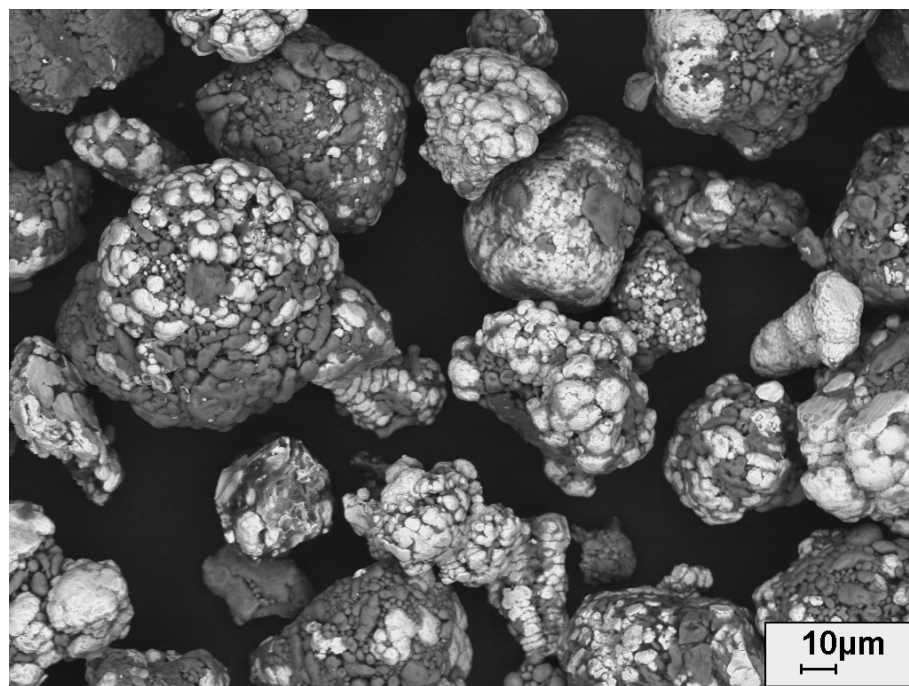


Figure 5: Scanning electron micrograph of an aluminum *clad* nickel powder (Ni5Al)

Content

Metals and metallic alloys

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| Copper Base | 13 |
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Cermets (Metal-ceramic composites)

| | |
|--|----|
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| Chromium carbide base | 27 |
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Oxide ceramics

| | |
|---------------|----|
| Alumina base | 28 |
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| Titania base | 32 |
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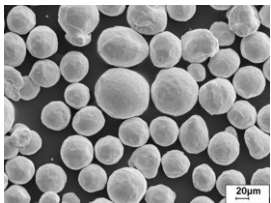
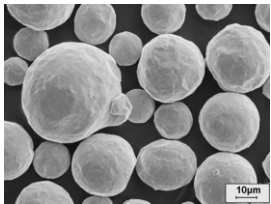
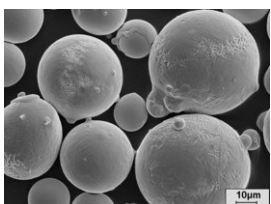
Polymers

| | |
|-----------|----|
| PTFE base | 34 |
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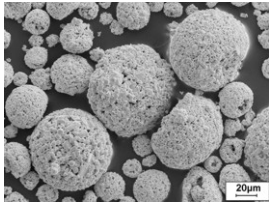
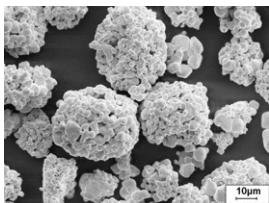
Metals and metallic alloys

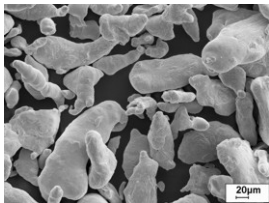
| | chemical composition | GTV number | particle size | spraying process | properties / application fields |
|---|----------------------------------|------------|------------------|------------------|--|
| Materials based on aluminum | | | | | |
| Al, water atomized | Al 99.0% | 30.54.1 | +20 µm -45 µm | APS | <ul style="list-style-type: none">Repair of aluminum and magnesium alloysCorrosion protection for pH 5 - 8,3, even at elevated temperature |
|  | | 30.54.2 | +45 µm -90 µm | PFS | |
| Materials based on copper | | | | | |
| Cu, water atomized | Cu 99.0% | 30.55.2 | +45 µm -90 µm | PFS | <ul style="list-style-type: none">Repair of copper and copper alloysHigh electrical conductivityHigh thermal conductivity |
| Cu/Al, clad powder | Al 10% Cu rest (Metco 445) | 20.45.2 | +45 µm -90 µm | PFS | <ul style="list-style-type: none">Bearing material featuring excellent gliding and dry-running operation properties„Self bonding“ due to chem. reaction of componentsApplicable up to about 230 °C |
| CuAlFe, gas atomized | Al 10% Fe 1% Cu rest | 30.51.2 | +45 µm -90 µm | PFS | <ul style="list-style-type: none">Repair of copper and copper alloysBearing material featuring excellent gliding and dry-running operation propertiesApplicable up to about 230 °C |

Specified powder represent a selection only.
We ask for your detailed enquiry.

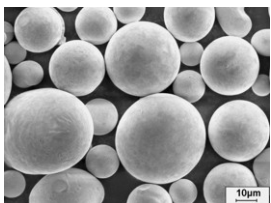
| | chemical composition | GTV number | particle size | spraying process | properties / application fields |
|---|---|------------|------------------|------------------|---|
| Materials based on iron | | | | | |
| Chromium steel, gas atomized | Cr 13.5% C 0.45% Fe rest | 80.91.8 | +15 µm -45 µm | HVOF APS | <ul style="list-style-type: none"> • Machinable steel for repair and build-up • Hardness: 34 HRC |
| Chromium steel, gas atomized | Cr 16% Ni 2% C 0.2% Fe rest | 30.42.2 | +45 µm -90 µm | PFS APS | <ul style="list-style-type: none"> • Machinable steel for repair and build-up • Hardness: 35 HRC |
| Aluminum-Molybdenum-Steel, clad powder | Al 10% Mo 1% C 0.2% Fe rest | 20.48.2 | +45 µm -90 µm | PFS APS | <ul style="list-style-type: none"> • Low shrinkage machinable steel for repair and build-up • „Self bonding“ due to chem. reaction of components • Hardness: 45 HRC • Applicable up to about 370 °C |
| Chromium-Nickel-Steel, gas atomized (AISI 316L)   | Cr 17% Ni 12.5% Mo 2.5% Si 0.7% Mn 1.5% C 0.02% Fe rest | 30.46.2 | +45 µm -90 µm | PFS APS | <ul style="list-style-type: none"> • Machinable austenitic steel for repair and build-up • High corrosion resistance in various media • Applicable up to about 540 °C |
| | | 80.46.1 | +20 µm -45 µm | HVOF | |
| Iron based hard alloy, gas atomized  | Cr 27% Ni 11% Mo 4% Si 1.5% C 2.0% Fe rest | 81.43.8S | +15 µm -53 µm | HVOF | <ul style="list-style-type: none"> • Corrosion protective coatings with excellent corrosion resistance in various media • Coating hardness 700 HV0,3 |

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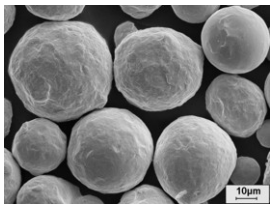
| | chemical composition | GTV number | particle size | spraying process | properties / application fields |
|---|--|-----------------|------------------|------------------|--|
| Materials based on molybdenum | | | | | |
| Mo, agglomerated and sintered   | Mo 99.0% O 0.1% | 30.63.2 | +45 µm -90 µm | PFS APS | <ul style="list-style-type: none"> • High adhesion strength due to high particle temperature and strong chemical reactivity • High resistance against all kinds of wear stress with excellent sliding properties • Coating hardness depending on oxidation 300 - 600 HV0,3 • Applicable up to about 320 °C (for excessive temperature oxidation) |
| | | 80.63.1 | +20 µm -53 µm | HVOF | |
| | | 80.63.1S | +15 µm -45 µm | HVOF | |
| Mo / NiCrBSi, powder blend | Ni 18% Cr 4.5% B 0.8% Si 2% Fe 1% Mo rest | 30.05.2 | +45 µm -90 µm | PFS | <ul style="list-style-type: none"> • High resistance against all kinds of wear stress • Hardness: 55 HRC • Applicable up to about 320 °C (for excessive temperature oxidation) |
| | | 80.05.1 | +20 µm -45 µm | APS HVOF | |

| | | | | | |
|--|-----------------|----------------|------------------|-----|---|
| Materials based on zinc | | | | | |
| Zn, water atomized  | Zn 99.0% | 30.10.2 | +45 µm -90 µm | PFS | <ul style="list-style-type: none"> • Corrosion protection for pH 7 - 12.5, at maximum temperature of 60 °C |

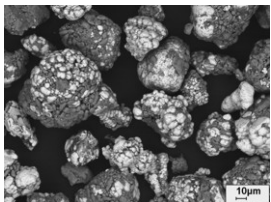
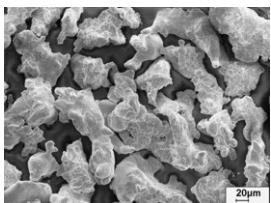
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| | chemical composition | GTV number | particle size | spraying process | properties / application fields |
|---|---|----------------|-------------------|------------------|--|
| Materials based on cobalt | | | | | |
| CoCrW, gas atomized  | Cr 30% W 12% C 2.5% Co rest (Stellite® 1) | 10.01.6 | +45 µm -125 µm | PFS APS | <ul style="list-style-type: none"> • High resistance against all kinds of wear stress • Good sliding properties • High impact resistance • High hot gas corrosion and oxidation resistance • Excellent corrosion resistance in various media • Hardness: HRC 54 • Applicable up to about 730 °C |
| | | 85.01.1 | +20 µm -45 µm | HVOF | |
| CoCrW, gas atomized | Cr 28% W 4% C 1.1% Co rest (Stellite® 6) | 15.06.6 | +45 µm -125 µm | PFS APS | <ul style="list-style-type: none"> • High resistance against all kinds of wear stress • Good sliding properties • High impact resistance • High hot gas corrosion and oxidation resistance • Excellent corrosion resistance in various media • Hardness: HRC 42 • Applicable up to about 730 °C |
| | | 85.06.1 | +20 µm -45 µm | HVOF | |
| CoCrW, gas atomized | Cr 28% W 8% C 1.5% Co rest (Stellite® 12) | 15.12.6 | +45 µm -125 µm | PFS APS | <ul style="list-style-type: none"> • High resistance against all kinds of wear stress • Good sliding properties • High impact resistance • High hot gas corrosion and oxidation resistance • Excellent corrosion resistance in various media • Hardness: HRC 48 • Applicable up to about 730 °C |
| | | 85.12.1 | +20 µm -45 µm | HVOF | |
| CoNiCrAlY, gas atomized | Ni 32% Cr 21% Al 8% Y 0.5% Co rest | 60.95.1 | +20 µm -45 µm | HVOF VPS | <ul style="list-style-type: none"> • Repair of super alloys with comparable composition • Excellent hot gas corrosion and oxidation resistance • Excellent corrosion resistance in various media • Applicable up to about 1050 °C |

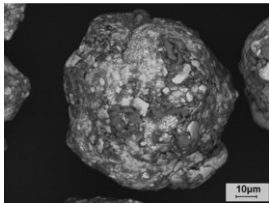
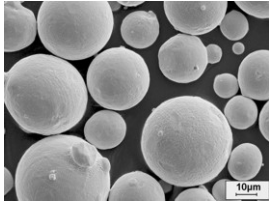
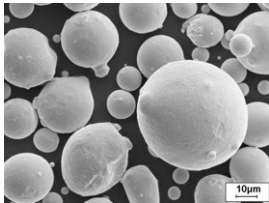
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| | chemical composition | GTV number | particle size | spraying process | properties / application fields |
|---|---------------------------------------|------------|-------------------|------------------|--|
| Materials based on nickel I | | | | | |
| Ni, water atomized | Ni 99.0% | 80.56.1 | +20 µm -45 µm | APS HVOF | <ul style="list-style-type: none"> • Machinable material for repair and build-up of nickel and nickel based alloys • Good corrosion resistance in various media |
| NiCr, gas atomized  | Cr 20% Ni rest | 80.20.1 | +20 µm -53 µm | APS HVOF | <ul style="list-style-type: none"> • Excellent bond coat for ceramic top coats • Machinable material for repair and build-up • High hot gas corrosion and oxidation resistance • Excellent corrosion resistance in various media • Applicable up to about 1000 °C |
| | | 80.20.0 | +10 µm -30 µm | APS HVOF | |
| | | 20.43.2 | +45 µm -90 µm | PFS | |
| Ni/Cr, clad powder | Cr 6% Ni rest | 60.43.6 | +45 µm -125 µm | APS | <ul style="list-style-type: none"> • Excellent bond coat for ceramic top coats • Machinable material for repair and build-up • High hot gas corrosion and oxidation as well as general corrosion resistance • Applicable up to about 1000 °C |
| NiCrAl, gas atomized | Cr 18% Al 6% Ni rest | 80.01.1 | +20 µm -53 µm | APS HVOF | <ul style="list-style-type: none"> • Excellent bond coat for ceramic top coats • Machinable material for repair and build-up • High hot gas corrosion and oxidation as well as general corrosion resistance • Applicable up to about 1000 °C |
| | | 30.01.2 | +45 µm -90 µm | PFS | |
| NiCrFe, gas atomized | Cr 16% Fe 9% Si 0.5% Ni rest | 30.04.2 | +45 µm -90 µm | PFS | <ul style="list-style-type: none"> • Excellent bond coat for ceramic top coats • Machinable material for repair and build-up • High hot gas corrosion and oxidation as well as general corrosion resistance • Applicable up to about 870 °C |

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| | chemical composition | GTV number | particle size | spraying process | properties / application fields |
|---|---|------------|------------------|------------------|---|
| Materials based on nickel II | | | | | |
| NiCrMoAl, clad powder (Metco 442) | Cr 8.5% Al 7% Mo 5% Si 2% B 2% Fe 2 % TiO ₂ 3 % Ni rest | 20.42.2 | +45 µm -90 µm | PFS | <ul style="list-style-type: none"> • Material for repair and build-up with limited machinability • High wear resistance • Good corrosion resistance in various media • „Self bonding“ due to chem. reaction of components • Hardness: HRC 35 • Applicable up to about 750 °C |
| NiCrMoAlFe, clad powder (Metco 444) | Cr 9% Al 7% Mo 5.5% Fe 5% Ni rest | 20.44.2 | +45 µm -90 µm | PFS | <ul style="list-style-type: none"> • Machinable material for repair and build-up • High wear resistance • Good corrosion resistance in various media • „Self bonding“ due to chem. reaction of components • Applicable up to about 870 °C |
| Ni/Al, clad powder  | Al 5% Ni rest | 20.50.2 | +45 µm -90 µm | PFS | <ul style="list-style-type: none"> • Machinable material for repair and build-up • Excellent bond coat for ceramic top coats with high ductility and impact resistance • Good corrosion resistance in various media • „Self bonding“ due to chem. reaction of components • Applicable up to about 800 °C |
| NiAl, water atomized  | Al 5% Ni rest | 21.50.2 | +45 µm -90 µm | PFS APS | <ul style="list-style-type: none"> • Machinable material for repair and build-up • Excellent bond coat for ceramic top coats with high ductility and impact resistance • Good corrosion resistance in various media • Applicable up to about 800 °C |
| NiAl, water atomized | Al 31% Ni rest | 21.69.1 | +20 µm -45 µm | APS | <ul style="list-style-type: none"> • Good corrosion resistance in various media • Good hot gas corrosion resistance • Applicable up to about 800 °C |

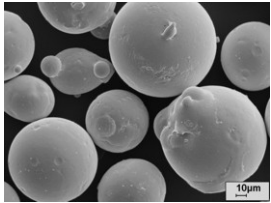
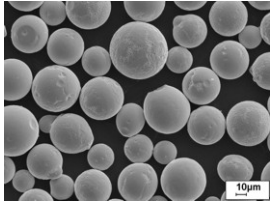
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| | chemical composition | GTV number | particle size | spraying process | properties / application fields |
|--|---|----------------|------------------|------------------|--|
| Materials based on nickel III | | | | | |
| NiAlMo, clad powder  | Al 5.5% Mo 5% Ni rest (Metco 447) | 20.47.2 | +45 µm -90 µm | PFS APS | <ul style="list-style-type: none"> • Machinable material for repair and build-up • High wear resistance • High ductility and impact resistance • Good corrosion resistance in various media • „Self bonding“ due to chem. reaction of components |
| NiCrAlY, gas atomized | Cr 22% Al 10% Y 1% Ni rest | 60.46.8 | +15 µm -38 µm | HVOF VPS | <ul style="list-style-type: none"> • Repair of super alloys with comparable composition • Excellent hot gas corrosion resistance • Excellent corrosion resistance in various media • Applicable up to about 1050 °C |
| NiCrMoNb, gas atomized  | Cr 21% Mo 9% Nb 3.5% Ni rest (Inconel® 625) | 80.25.1 | +20 µm -53 µm | APS HVOF | <ul style="list-style-type: none"> • Machinable material for repair and build-up of super alloys with comparable composition • High wear resistance • Good hot gas corrosion resistance • Excellent corrosion resistance in various media • Applicable up to about 800 °C |
| NiCrMoW, gas atomized  | Cr 16% Mo 16% W 4% Fe 5.5% Ni rest (Hastalloy® C / C-276) | 80.93.1 | +20 µm -53 µm | APS HVOF | <ul style="list-style-type: none"> • Machinable material for repair and build-up of super alloys with comparable composition • High wear resistance • Good hot gas corrosion resistance • Excellent corrosion resistance in various media • Applicable up to about 800 °C |

Specified powder represent a selection only.
We ask for your detailed enquiry.

| | chemical composition | GTV number | particle size | spraying process | properties / application fields |
|--|---|------------|-------------------|------------------|---|
| Materials based on nickel (Self fluxing alloys) I | | | | | |
| NiBSi, gas atomized | B 1.3% Si 2.3% Fe 1% Ni rest HRC 22 | 10.10.5 | +30 µm -105 µm | PFS APS | <ul style="list-style-type: none"> • High wear resistance • Good corrosion resistance in various media • Good machinability |
| | | 10.10.6 | +45 µm -125 µm | PFS APS | <ul style="list-style-type: none"> • After fusion coatings are gas tight and metallurgically bonded to substrates due to diffusion • Hardness: HRC 22-25 • Applicable up to about 820 °C |
| NiCrBSi, gas atomized | Cr 7% B 1.25 Si 3.4% Fe 3% C 0.15% Ni rest HRC 30 | 10.11.5 | +30 µm -105 µm | PFS APS | <ul style="list-style-type: none"> • High wear resistance • Good corrosion resistance in various media • Good machinability • After fusion coatings are gas tight and metallurgically bonded to substrates due to diffusion • Hardness: HRC 33-35 • Applicable up to about 820 °C |
| NiCrBSi, gas atomized | Cr 7.5% B 1.7% Si 3.5% Fe 2.5% C 0.25% Ni rest HRC 40 | 10.12.6 | +45 µm -125 µm | PFS APS | <ul style="list-style-type: none"> • High wear resistance • Good corrosion resistance in various media • Good machinability • After fusion coatings are gas tight and metallurgically bonded to substrates due to diffusion • Hardness: HRC 30-35 • Applicable up to about 820 °C |
| NiCrBSi, gas atomized | Cr 14% B 2.5% Si 3.7% Fe 4% C 0.5% Ni rest HRC 50 | 10.14.6 | +45 µm -125 µm | PFS APS | <ul style="list-style-type: none"> • High wear resistance • Good corrosion resistance in various media • Good machinability • After fusion coatings are gas tight and metallurgically bonded to substrates due to diffusion • Low susceptibility to cracking • Hardness: HRC 48-50 • Applicable up to about 820 °C |

Specified powder represent a selection only.
We ask for your detailed enquiry.

| | chemical composition | GTV number | particle size | spraying process | properties / application fields |
|---|---|------------|-------------------|------------------|--|
| Materials based on nickel (Self fluxing alloys) II | | | | | |
| NiCrBSi, water atomized | Cr 14% B 3.3% | 10.15.6 | +45 µm -125 µm | PFS APS | <ul style="list-style-type: none"> • High wear resistance • Good corrosion resistance in various media • High impact resistance • After fusion coatings are gas tight and metallurgically bonded to substrates due to diffusion • Hardness: HRC 60-62 • Applicable up to about 820 °C |
| NiCrBSi, gas atomized | Si 4.5% Fe 4.5% C 0.75% Ni rest HRC 60 | 10.15.6G | +45 µm -125 µm | PFS APS | |
|   | | 80.15.1 | +20 µm -53 µm | HVOF | |
| NiCrBSiCuMo, gas atomized | Cr 16% B 3.5% Si 4.5% Fe 3.5% Cu 3% Mo 3% C 0.5% Ni rest HRC 58 | 10.16.6 | +45 µm -125 µm | PFS APS | <ul style="list-style-type: none"> • High wear resistance • Good corrosion resistance in various media • High impact resistance, maximum edge stability • After fusion coatings are gas tight and metallurgically bonded to substrates due to diffusion • Hardness: HRC 58 • Applicable up to about 820 °C |
| NiCrBSiFeMoCo, gas atomized | no declaration HRC 52 | 10.18.6 | +45 µm -125 µm | PFS APS | <ul style="list-style-type: none"> • High wear resistance • Good corrosion resistance in various media • High impact resistance • After fusion coatings are gas tight and metallurgically bonded to substrates due to diffusion • Hardness: HRC 52 • Applicable up to about 760 °C |

Specified powder represent a selection only.

We ask for your detailed enquiry.

Cermets (Metal-Ceramic Composites)

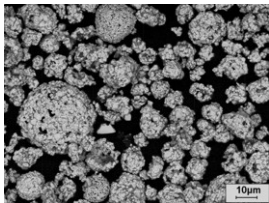
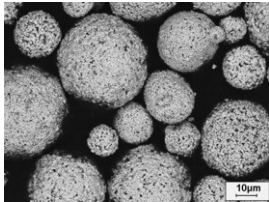
| | chemical composition | GTV number | particle size | spraying process | properties / application fields |
|---|----------------------------|------------|-------------------|------------------|--|
| Self fluxing alloys with carbide reinforcement | | | | | |
| NiCrBSi, WC/Co 88/12, powder blend | 80.15.1 20% 80.71.1 80% | 80.32.1 | +20 µm -45 µm | HVOF APS | <ul style="list-style-type: none"> • High wear resistance • Good corrosion resistance in various media • High impact resistance • Applicable up to about 540 °C |
| | 10.15.6 20% 10.71.2 80% | 10.32.6 | +45 µm -125 µm | PFS APS | |
| NiCrBSi, WC/Ni 88/12, powder blend | 80.15.1 50% 80.77.1 50% | 80.34.1 | +20 µm -45 µm | HVOF APS | <ul style="list-style-type: none"> • High wear resistance • Good corrosion resistance in various media • High impact resistance • More ductile than 80.32.1 / 10.32.6 • Applicable up to about 540 °C |
| | 10.15.6 50% 10.77.2 50% | 10.34.5 | +30 µm -105 µm | PFS APS | |
| | | 10.34.6 | +45 µm -125 µm | PFS APS | |
| NiCrBSi, WC/Ni 88/12, powder blend | 10.15.6 65% 10.77.2 35% | 10.36.6 | +45 µm -125 µm | PFS APS | <ul style="list-style-type: none"> • High wear resistance • Good corrosion resistance in various media • High impact resistance • More ductile than 10.34.6 • Applicable up to about 540 °C |
| NiCrBSi, WC/Ni 88/12, powder blend | 10.15.6 35% 10.77.2 65% | 10.37.6 | +45 µm -125 µm | PFS APS | <ul style="list-style-type: none"> • High wear resistance • Good corrosion resistance in various media • High impact resistance • Applicable up to about 540 °C |
| NiCrBSi, Cr ₃ C ₂ /Ni 25/75, powder blend | 10.15.6 25% 10.81.2 75% | 10.81.2 | +45 µm -125 µm | PFS APS | <ul style="list-style-type: none"> • High wear resistance • Good corrosion resistance in various media • High impact resistance • Applicable up to about 820 °C |

Specified powder represent a selection only.

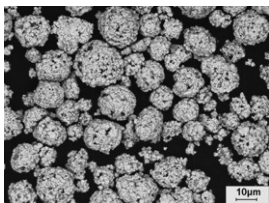
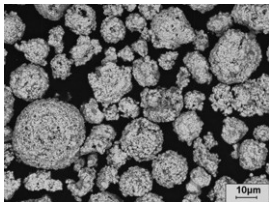
We ask for your detailed enquiry.

| | chemical composition | GTV number | particle size | spraying process | properties / application fields |
|--|----------------------------|------------|------------------|------------------|---|
| Nickel based alloys with oxide reinforcement | | | | | |
| NiAl, ZrO ₂ /Y ₂ O ₃ 92/8, powder blend | 20.50.2 35% 40.23.4 65% | 40.12.4 | +15 µm -90 µm | APS | <ul style="list-style-type: none"> • High wear resistance • Good corrosion resistance in various media • Bond strength, impact and thermal shock resistance better than for pure ceramic coatings • Applicable up to about 800 °C |
| NiAl, ZrO ₂ /Y ₂ O ₃ 92/8, powder blend | 20.50.2 65% 40.23.4 35% | 40.13.4 | +15 µm -90 µm | APS | <ul style="list-style-type: none"> • High wear resistance • Good corrosion resistance in various media • Bond strength, impact and thermal shock resistance better than for pure ceramic coatings • Applicable up to about 800 °C |
| NiAl, ZrO ₂ /MgO 80/20, powder blend | 20.50.2 35% 40.21.4 65% | 40.14.4 | +15 µm -90 µm | APS | <ul style="list-style-type: none"> • High wear resistance • Good corrosion resistance in various media • Bond strength, impact and thermal shock resistance better than for pure ceramic coatings • Applicable up to about 800 °C |

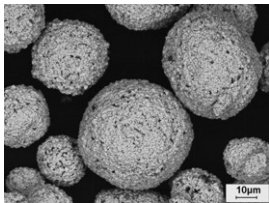
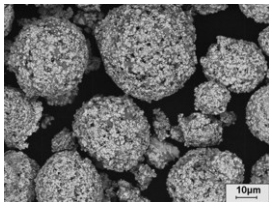
Specified powder represent a selection only.
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| | chemical composition | GTV number | particle size | spraying process | properties / application fields |
|--|------------------------------------|-------------------|-------------------|------------------|---|
| Materials based on tungsten carbide I | | | | | |
| WC/Co 88/12, agglomerated and sintered   | Co 12% C 4% W rest | 80.71.0W20 | +5 µm -20 µm | HVOF | <ul style="list-style-type: none"> • Excellent wear resistance • Suitable for replacement of electroplated hard chromium in non-corrosive media • Coating hardness 800-1400 HV0,3 • Applicable up to about 540 °C |
| | | 80.71.0 | +5 µm -25 µm | HVOF | |
| | | 80.71.1 | +20 µm -45 µm | HVOF APS | |
| | | 80.71.1W | +20 µm -53 µm | HVOF APS | |
| | | 80.71.3W | +5 µm -45 µm | HVOF APS | |
| | | 80.71.8S | +10 µm -40 µm | HVOF APS | |
| | | 10.71.2 | +45 µm -90 µm | APS PFS | |
| | | 10.71.60W | +90 µm -125 µm | APS PFS | |
| | | 65.71.1-6P | +15 µm -53 µm | HVOF APS | |
| WC/Co 88/12, PTFE, powder blend | 65.00.1 6% 80.71.1W 94% | 65.71.1-6P | +15 µm -53 µm | HVOF APS | <ul style="list-style-type: none"> • Excellent wear resistance • Anti-sticking properties due to lower surface energy compared to 80.71 und 10.71 • Applicable up to about 260 °C |

Specified powder represent a selection only.
We ask for your detailed enquiry.

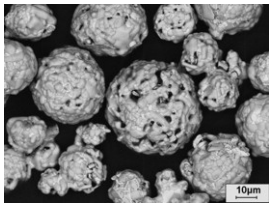
| | chemical composition | GTV number | particle size | spraying process | properties / application fields |
|--|---|-------------------|------------------|------------------|---|
| Materials based on tungsten carbide II | | | | | |
| WC/Co 83/17, agglomerated and sintered  | Co 17% C 5.2% W rest | 80.73.0W20 | +5 µm -20 µm | HVOF | <ul style="list-style-type: none"> • Excellent wear resistance • For adequate processing conditions higher ductility and lower hardness than 80.71 • Coating hardness 800-1400 HV0,3 • Applicable up to about 540 °C |
| | | 80.73.1 | +20 µm -45 µm | HVOF APS | |
| | | 80.73.1W | +20 µm -53 µm | HVOF APS | |
| | | | | | |
| WC/CoCr 86/10-4, agglomerated and sintered  | Co 10% Cr 4% C 5.3% W rest | 80.76.0W20 | +5 µm -20 µm | HVOF | <ul style="list-style-type: none"> • Excellent wear resistance • Improved corrosion resistance compared to 80.71 and 80.73 • Application in various media for pH > 4 possible • Superior to electroplated hard chromium in most properties • Coating hardness 800-1450 HV0,3 • Applicable up to about 540 °C |
| | | 80.76.0W | +5 µm -25 µm | HVOF | |
| | | 80.76.1 | +20 µm -45 µm | HVOF APS | |
| | | 80.76.8W | +10 µm -38 µm | HVOF APS | |
| | | | | | |

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| | chemical composition | GTV number | particle size | spraying process | properties / application fields |
|--|---|-----------------|------------------|------------------|--|
| Materials based on tungsten carbide III | | | | | |
| WC/Ni 88/12, agglomerated and sintered  | Ni 12% C 4.2% W rest | 80.77.1 | +20 µm -45 µm | HVOF APS | <ul style="list-style-type: none"> • Excellent wear resistance • Improved corrosion resistance compared to 80.71 in many media • Application in various media for pH > 5 possible • Coating hardness 1000-1200 HV0,3 • Applicable up to about 540 °C |
| | | 80.77.1W | +20 µm -53 µm | HVOF APS | |
| | | 10.77.2 | +45 µm -90 µm | APS PFS | |
| WC/Cr₃C₂/Ni 73/20/7, agglomerated and sintered  | Ni 7% Cr 21% C 5.7% W rest | 80.75.1 | +20 µm -45 µm | HVOF APS | <ul style="list-style-type: none"> • Excellent wear resistance • Improved corrosion resistance compared to 80.71 in many media • Application in various media for pH > 4 possible • Coating hardness 1000-1200 HV0,3 • Applicable up to about 540 °C |
| | | 80.75.1X | +15 µm -45 µm | HVOF APS | |

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| | chemical composition | GTV number | particle size | spraying process | properties / application fields |
|---|----------------------------|-------------|------------------|------------------|--|
| Materials based on chromium carbide | | | | | |
| $\text{Cr}_3\text{C}_2/\text{Ni20Cr 75/25}$, agglomerated and sintered  | Ni 20% C 10% Cr rest | 80.81.1 | +20 µm -45 µm | HVOF APS | <ul style="list-style-type: none"> • Excellent combined wear and corrosion resistance in various media • Coating hardness 800-1300 HV0,3 • Applicable up to about 980 °C |
| | | 80.81.1W | +20 µm -53 µm | HVOF APS | |
| | | 80.81.3W | +5 µm -45 µm | HVOF APS | |
| | | 80.81.8W | +10 µm -38 µm | HVOF APS | |
| | | 10.81.2 | +45 µm -90 µm | APS PFS | |
| $\text{Cr}_3\text{C}_2/\text{Ni20Cr 75/25}$, PTFE, powder blend | PTFE 10% 80.81.1 90% | 65.81.1-10P | +20 µm -45 µm | HVOF APS | <ul style="list-style-type: none"> • Excellent wear resistance • Anti-sticking properties due to lower surface energy compared to 80.81 und 10.81 • Applicable up to about 260 °C |

| | | | | | |
|---|-------------------------|---------|-------------------|-----|--|
| Materials based on graphite | | | | | |
| Ni/graphite 85/15 , clad powder | graphite 15% Ni rest | 60.08.5 | +30 µm -105 µm | APS | <ul style="list-style-type: none"> • Excellent abradable coating • Good sliding properties • Long term applicability for temperatures up to about 480°C |

Specified powder represent a selection only.
We ask for your detailed enquiry.

Oxide ceramics

| | chemical composition | GTV number | particle size | spraying process | properties / application fields |
|---|--|------------|------------------|----------------------------|---|
| Materials based on alumina I | | | | | |
| Al ₂ O ₃ , fused and crushed | Al ₂ O ₃ 99,0% | 40.05.0 | +5 µm -25 µm | HVOF _{Gas} APS | <ul style="list-style-type: none"> • High wear resistance except for fatigue load conditions • Coating hardness 600-1200 HV0,3 • Applicable up to about 1500 °C • Excellent dielectric strength, especially at elevated temperature • Electr. resistance: 10¹⁵ Wcm • High chemical resistance except for bases |
| | | 40.05.1 | +15 µm -45 µm | APS | |
| Al ₂ O ₃ /TiO ₂ 97/3, fused and crushed | TiO ₂ 3% Al ₂ O ₃ Rest | 40.01.0 | +5 µm -25 µm | HVOF _{Gas} APS | <ul style="list-style-type: none"> • High chemical resistance except for bases • High wear resistance except for fatigue load conditions • Higher ductility than 40.05 • Lower roughness than for 40.05 possible after grinding • Coating hardness 600-1100 HV0,3 • Applicable up to about 1100 °C |
| | | 40.01.1 | +20 µm -45 µm | APS | |
| | | 40.01.4 | +15 µm -60 µm | APS | |
| | | 40.01.8 | +10 µm -40 µm | APS | |

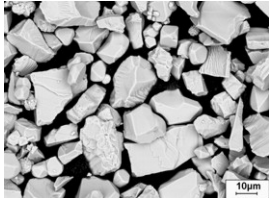
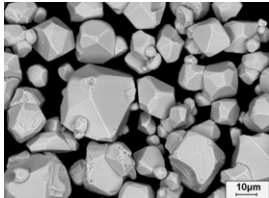
Specified powder represent a selection only.
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| | chemical composition | GTV number | particle size | spraying process | properties / application fields |
|--|---|------------|------------------|----------------------------|---|
| Materials based on alumina II | | | | | |
| Al ₂ O ₃ /TiO ₂ 87/13, fused and crushed | TiO ₂ 13% Al ₂ O ₃ rest | 40.30.0 | +5 µm -25 µm | HVOF _{Gas} APS | <ul style="list-style-type: none"> • High chemical resistance except for bases • High wear resistance except for fatigue load conditions • Higher ductility than 40.01 • Lower roughness than for 40.01 possible after grinding (R_a = 0,2 µm) • Coating hardness 500-1000 HV0,3 • Applicable up to about 550 °C • Low wettability |
| | | 40.30.1 | +20 µm -45 µm | APS | |
| | | 40.30.4 | +15 µm -60 µm | APS | |
| Al ₂ O ₃ /TiO ₂ 60/40, fused and crushed | TiO ₂ 40% Al ₂ O ₃ rest | 40.31.0 | +5 µm -25 µm | HVOF _{Gas} APS | <ul style="list-style-type: none"> • Lower chemical resistance than 40.30 • High wear resistance except for fatigue load conditions • Higher ductility than 40.30 • Lower roughness than for 40.30 possible after grinding • Coating hardness 400-1000 HV0,3 • Applicable up to about 550 °C • Low wettability |
| | | 40.31.1 | +20 µm -45 µm | APS | |
| | | 40.31.4 | +15 µm -60 µm | APS | |
| Al ₂ O ₃ /TiO ₂ 50/50, fused and crushed | TiO ₂ 50% Al ₂ O ₃ rest | 40.33.0 | +5 µm -25 µm | HVOF _{Gas} APS | <ul style="list-style-type: none"> • Lower chemical resistance than 40.31 • High wear resistance except for fatigue load conditions • Higher ductility than 40.31 • Lower roughness than for 40.31 possible after grinding • Coating hardness 400-900 HV0,3 • Applicable up to about 550 °C • Low wettability |
| | | 40.33.1 | +20 µm -45 µm | APS | |
| | | 40.33.4 | +15 µm -60 µm | APS | |

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| | chemical composition | GTV number | particle size | spraying process | properties / application fields |
|---|---|-------------|------------------|----------------------------|--|
| Materials based on alumina III | | | | | |
| Al ₂ O ₃ /ZrO ₂ 75/25, fused and crushed | ZrO ₂ 25% Al ₂ O ₃ rest | 40.28.1 | +20 µm -45 µm | APS | <ul style="list-style-type: none"> • High wear resistance except for fatigue load conditions • Applicable up to about 1300 °C |
| Al ₂ O ₃ /MgO 72/28, fused and crushed | MgO 28% Al ₂ O ₃ rest | 40.29.1 | +20 µm -45 µm | APS | <ul style="list-style-type: none"> • High wear resistance except for fatigue load conditions • Applicable up to about 900 °C |
| Al ₂ O ₃ /TiO ₂ /PTFE, powder blend | PTFE 10% TiO ₂ 11.7% Al ₂ O ₃ rest | 65.30.1-10P | +20 µm -45 µm | HVOF _{Gas} APS | <ul style="list-style-type: none"> • High wear resistance except for fatigue load conditions • Lower surface energy compared to pure ceramic coatings, therefore anti-sticking property • Applicable up to about 260 °C |

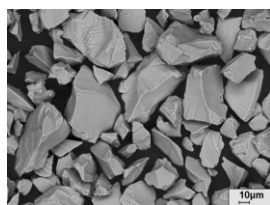
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| | chemical composition | GTV number | particle size | spraying process | properties / application fields |
|--|--|----------------|------------------|----------------------------|---|
| Materials based on chromia I | | | | | |
| Cr₂O₃, fused and crushed  | Cr₂O₃ 97% | 40.06.0 | +5 µm -25 µm | HVOF _{Gas} APS | <ul style="list-style-type: none"> • High chemical resistance for all pH values • High wear resistance except for fatigue load conditions • Low roughness possible after grinding (R_a = 0,1 µm) • Electr. resistance: 10⁷ Wcm • Coating hardness 1500 HV0,3 • Applicable up to about 500 °C |
| | | 40.06.1 | +20 µm -45 µm | APS | |
| | | 40.06.4 | +15 µm -60 µm | APS | |
| Cr₂O₃, fused and crushed  | Cr₂O₃ 99.6% | 41.06.0 | +5 µm -25 µm | HVOF _{Gas} APS | <ul style="list-style-type: none"> • High chemical resistance for all pH values • High wear resistance except for fatigue load conditions • Low roughness possible after grinding (R_a = 0,1 µm) • Electr. resistance: 10⁷ Wcm • Coating hardness 1500 HV0,3 • Applicable up to about 500 °C • Higher purity than 40.06; metal free, therefore laser engraving possible |
| | | 41.06.1 | +20 µm -45 µm | APS | |
| | | 41.06.8 | +15 µm -38 µm | APS | |

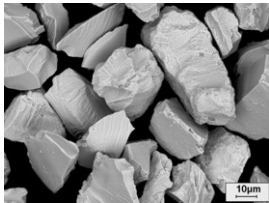
Specified powder represent a selection only.
We ask for your detailed enquiry.

| | chemical composition | GTV number | particle size | spraying process | properties / application fields |
|---|---|------------|------------------|----------------------------|---|
| Materials based on chromia II | | | | | |
| Cr ₂ O ₃ /TiO ₂ 60/40, fused and crushed | TiO ₂ 40% Cr ₂ O ₃ rest | 40.60.1 | +20 µm -45 µm | APS | <ul style="list-style-type: none"> • High wear resistance except for fatigue load conditions • Improved ductility compared to pure Cr₂O₃ coatings • Coating hardness 600 HV0,3 • Applicable up to about 500 °C • Low roughness possible after grinding |
| Cr ₂ O ₃ /SiO ₂ /TiO ₂ 92/5/3, fused and crushed | SiO ₂ 5% TiO ₂ 3% Cr ₂ O ₃ rest | 40.36.0 | +5 µm -25 µm | HVOF _{Gas} APS | <ul style="list-style-type: none"> • High chemical resistance for all pH values • High wear resistance except for fatigue load conditions • More impact resistant than pure Cr₂O₃ coatings |
| | | 40.36.1 | +20 µm -45 µm | APS | <ul style="list-style-type: none"> • Coating hardness 900-1300 HV0,3 • Applicable up to about 500 °C |

| | | | | | |
|---|----------------------|---------|------------------|-----|--|
| Materials based on titania | | | | | |
| TiO ₂ , fused and crushed | TiO ₂ 97% | 40.02.1 | +20 µm -45 µm | APS | <ul style="list-style-type: none"> • Good wear resistance (however, lower compared to alumina or chromia based coatings) except for fatigue load conditions • Improved ductility compared to Cr₂O₃ coatings • Coating hardness 650 HV0,3 • Applicable up to about 500 °C • antistatic |



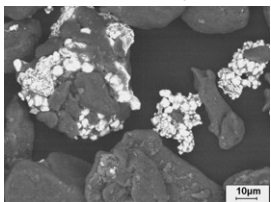
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| | chemical composition | GTV number | particle size | spraying process | properties / application fields |
|---|--|------------|-------------------|------------------|---|
| Materials based on zirconia I | | | | | |
| ZrO₂/Y₂O₃ 92/8, fused and crushed  | Y₂O₃ 8% ZrO ₂ rest | 40.23.1 | +20 µm -45 µm | APS | <ul style="list-style-type: none"> • Optimum coating material for heat insulation due to low thermal conductivity and excellent thermal shock resistance • Low thermal expansion mismatch to super alloys ($11 \cdot 10^{-6} \cdot K^{-1}$) • Coating hardness 500 HV0,3 • In combination with MCrAlY bond coats on super alloys long term applicability for surface temperatures up 1250 °C • Electr. Resistance: 10^{11} Wcm • Suitable for clearance control |
| | | 40.23.4 | +15 µm -60 µm | APS | |
| | | 40.23.5N | +45 µm -100 µm | APS | |
| ZrO₂/Y₂O₃ 92/8, agglomerated and sintered | Y₂O₃ 8% ZrO ₂ rest | | | | |
| ZrO₂/Y₂O₃ 87/13, fused and crushed | Y₂O₃ 13% ZrO ₂ rest | 40.24.1 | +20 µm -45 µm | APS | <ul style="list-style-type: none"> • Low thermal conductivity • High thermal shock resistance, but inferior to 40.23 • Therm. expansion: $11 \cdot 10^{-6} \cdot K^{-1}$ • Coatings hardness 500 HV0,3 • Applicable up to about 1150 °C • Suitable for clearance control |
| ZrO₂/MgO 80/20, fused and crushed | MgO 20% ZrO ₂ rest | 40.21.1 | +20 µm -45 µm | APS | <ul style="list-style-type: none"> • Low thermal conductivity • High thermal shock resistance, but inferior to 40.23 • Coatings hardness 300-800 HV0,3 • Applicable up to about 900 °C • Suitable for clearance control |
| ZrO₂/CaO 95/5, fused and crushed | CaO 5% ZrO ₂ rest | 40.20.1 | +20 µm -45 µm | APS | <ul style="list-style-type: none"> • Low thermal conductivity • High thermal shock resistance, but inferior to 40.23 • Coatings hardness 300-600 HV0,3 • Applicable up to about 900 °C • Suitable for clearance control |

Specified powder represent a selection only.
We ask for your detailed enquiry.

| | chemical composition | GTV number | particle size | spraying process | properties / application fields |
|--|----------------------------------|------------|------------------|------------------|--|
| Materials based on zirconia II | | | | | |
| ZrO ₂ /CaO 70/30, fused and crushed | CaO 30% ZrO ₂ rest | 40.26.1 | +20 µm -45 µm | APS | <ul style="list-style-type: none"> • Low thermal conductivity • High thermal shock resistance, but inferior to 40.23 • Coatings hardness 400 HV0,3 • Applicable up to about 900 °C • Suitable for clearance control |

Polymers

| | | | | | |
|---|--|---------|------------------|-------------|---|
| Materials based on PTFE | | | | | |
| PTFE, clad by Mo  | Mo PTFE rest | 65.00.1 | +20 µm -45 µm | HVOF APS | <ul style="list-style-type: none"> • Powder for blends offering anti-sticking property coatings • Applicable up to about 260 °C |
| PTFE, clad by Ni | Ni PTFE rest | 65.00.1 | +20 µm -45 µm | HVOF APS | <ul style="list-style-type: none"> • Powder for blends offering anti-sticking property coatings • Applicable up to about 260 °C |
| PTFE, clad by Al ₂ O ₃ /TiO ₂ 97/3 | Al ₂ O ₃ /TiO ₂ 97/3 PTFE rest | 65.00.1 | +20 µm -45 µm | HVOF APS | <ul style="list-style-type: none"> • Powder for blends offering anti-sticking property coatings • Applicable up to about 260 °C |

Specified powder represent a selection only.
We ask for your detailed enquiry.